

# Velocity and acceleration

## GENERAL METHOD

$$f_1 = f_1(w_1, \dots, w_k, q_1, \dots, q_n, x_1, \dots, x_m) = 0$$

$$f_2 = f_2(w_1, \dots, w_k, q_1, \dots, q_n, x_1, \dots, x_m) = 0$$

...

$$f_m = f_m(w_1, \dots, w_k, q_1, \dots, q_n, x_1, \dots, x_m) = 0$$

**w** – vector of links' dimensions,

**q** – vector of known independent variables (drivers' position),

**x** – vector of unknown dependent variables (links' position)

$$\mathbf{f}(\mathbf{w}, \mathbf{q}, \mathbf{x}) = 0$$

$$\mathbf{q} = \mathbf{q}(t)$$

$$\mathbf{x} = \mathbf{x}(t)$$

$$f = 0 \rightarrow \frac{df}{dt} = 0 \rightarrow \frac{\partial f}{\partial \mathbf{x}} \dot{\mathbf{x}} + \frac{\partial f}{\partial \mathbf{q}} \dot{\mathbf{q}} = 0$$

$$\frac{\partial \mathbf{f}}{\partial \mathbf{x}} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} & \dots & \frac{\partial f_1}{\partial x_m} \\ \dots & \dots & \dots & \dots \\ \frac{\partial f_m}{\partial x_1} & \frac{\partial f_m}{\partial x_2} & \dots & \frac{\partial f_m}{\partial x_m} \end{bmatrix} = \mathbf{A}$$

$$\dot{\mathbf{x}} = [\dot{x}_1 \dots \dot{x}_m]^T$$

Dependent  
velocities

$$-\frac{\partial \mathbf{f}}{\partial \mathbf{q}} = - \begin{bmatrix} \frac{\partial f_1}{\partial q_1} & \frac{\partial f_1}{\partial q_2} & \cdots & \frac{\partial f_1}{\partial q_n} \\ \cdots & \cdots & \cdots & \cdots \\ \frac{\partial f_m}{\partial q_1} & \frac{\partial f_m}{\partial q_2} & \cdots & \frac{\partial f_m}{\partial q_n} \end{bmatrix} = \mathbf{B}$$

$$\dot{q} = [\dot{q}_1 \cdots \dot{q}_n]^T$$

Independent velocities, drivers

$$A\dot{x} = B\dot{q}$$

$$A^{-1}A = 1$$

$$\dot{x} = A^{-1}B\dot{q}$$

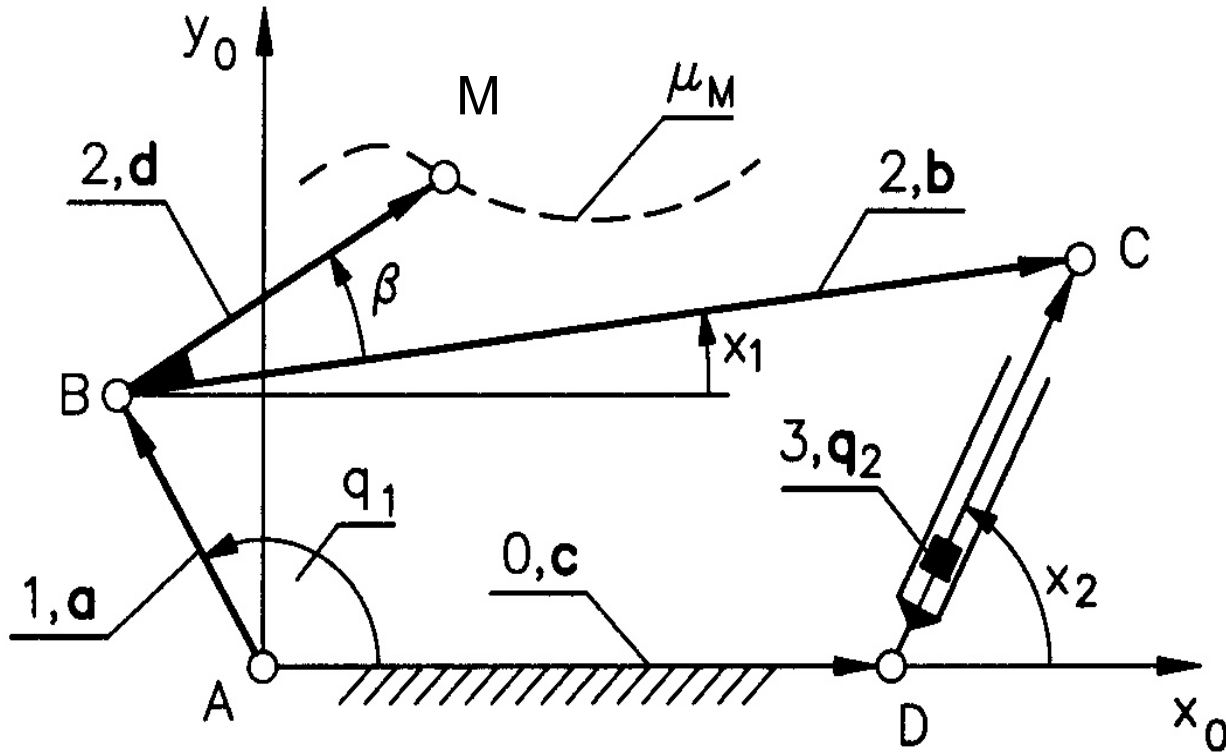
$$\ddot{x} = [\ddot{x}_1 \dots \ddot{x}_m]^T$$

$$\ddot{q} = [\ddot{q}_1 \dots \ddot{q}_n]^T$$

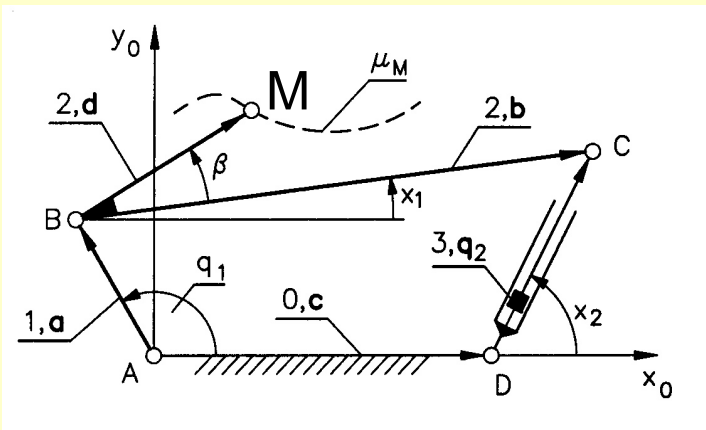
$$A\dot{x} = B\dot{q} \quad \longrightarrow \quad A\ddot{x} + \dot{A}\dot{x} = B\ddot{q} + \dot{B}\dot{q}$$

$$\ddot{x} = A^{-1}(-\dot{A}\dot{x} + \dot{B}\dot{q} + B\ddot{q})$$

## Example of 2 DOF manipulator



$$q_1, q_2 \rightarrow x_M = \quad y_M =$$



$$\mathbf{a} + \mathbf{b} - \mathbf{c} - \mathbf{q}_2 = \mathbf{0} \quad \rightarrow$$

$$\begin{aligned} a \cos q_1 + b \cos x_1 - c - q_2 \cos x_2 &= 0 \\ a \sin q_1 + b \sin x_1 - q_2 \sin x_2 &= 0 \end{aligned}$$

$$\mathbf{f} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix} = \begin{bmatrix} a \cos q_1 + b \cos x_1 - c - q_2 \cos x_2 \\ a \sin q_1 + b \sin x_1 - q_2 \sin x_2 \end{bmatrix} = \mathbf{0}$$

$q_1, q_2$  – independent (drivers),

$x_1, x_2$  – unknowns,

$$\mathbf{f} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix} = \begin{bmatrix} a \cos q_1 + b \cos x_1 - c - q_2 \cos x_2 \\ a \sin q_1 + b \sin x_1 - q_2 \sin x_2 \end{bmatrix} = \mathbf{0}$$

$$\frac{\partial \mathbf{f}}{\partial \mathbf{x}} = \begin{bmatrix} \frac{\partial f_1}{\partial x_1} & \frac{\partial f_1}{\partial x_2} & \cdots & \frac{\partial f_1}{\partial x_m} \\ \vdots & \vdots & \vdots & \vdots \\ \frac{\partial f_m}{\partial x_1} & \frac{\partial f_m}{\partial x_2} & \cdots & \frac{\partial f_m}{\partial x_m} \end{bmatrix} = \mathbf{A}$$

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$$\mathbf{A} = \frac{\partial \mathbf{f}}{\partial \mathbf{x}} = \begin{bmatrix} -b \sin x_1 & q_2 \sin x_2 \\ b \cos x_1 & -q_2 \cos x_2 \end{bmatrix}$$



$$\mathbf{f} = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix} = \begin{bmatrix} a \cos q_1 + b \cos x_1 - c - q_2 \cos x_2 \\ a \sin q_1 + b \sin x_1 - q_2 \sin x_2 \end{bmatrix} = \mathbf{0}$$

$$-\frac{\partial \mathbf{f}}{\partial \mathbf{q}} = - \begin{bmatrix} \frac{\partial f_1}{\partial q_1} & \frac{\partial f_1}{\partial q_2} & \cdots & \frac{\partial f_1}{\partial q_n} \\ \vdots & \vdots & \vdots & \vdots \\ \frac{\partial f_m}{\partial q_1} & \frac{\partial f_m}{\partial q_2} & \cdots & \frac{\partial f_m}{\partial q_n} \end{bmatrix} = \mathbf{B}$$

---

$$\mathbf{B} = -\frac{\partial \mathbf{f}}{\partial \mathbf{q}} = - \begin{bmatrix} -a \sin q_1 & -\cos x_2 \\ a \cos q_1 & -\sin x_2 \end{bmatrix}$$

$$\dot{\mathbf{x}} = \mathbf{A}^{-1} \mathbf{B} \dot{\mathbf{q}}$$

$$\dot{\mathbf{x}} = [\dot{x}_1 \ \dot{x}_2]^T \quad \dot{\mathbf{q}} = [\dot{q}_1 \ \dot{q}_2]^T$$

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Velocity equation

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -b \sin x_1 & q_2 \sin x_2 \\ b \cos x_1 & -q_2 \cos x_2 \end{bmatrix}^{-1} \begin{bmatrix} a \sin q_1 & \cos x_2 \\ -a \cos q_1 & \sin x_2 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

Velocity equation

$$\dot{\mathbf{x}} = \mathbf{A}^{-1} \mathbf{B} \dot{\mathbf{q}}$$



Acceleration equation

$$\ddot{\mathbf{x}} = \mathbf{A}^{-1} (-\dot{\mathbf{A}}\dot{\mathbf{x}} + \dot{\mathbf{B}}\dot{\mathbf{q}} + \mathbf{B}\ddot{\mathbf{q}})$$

$$\mathbf{A} = \frac{\partial \mathbf{f}}{\partial \mathbf{x}} = \begin{bmatrix} -b \sin x_1 & q_2 \sin x_2 \\ b \cos x_1 & -q_2 \cos x_2 \end{bmatrix}$$

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$$\dot{\mathbf{A}} = \frac{d}{dt} \mathbf{A} = \begin{bmatrix} -\dot{x}_1 b \cos x_1 & \dot{q}_2 \sin x_2 - \dot{x}_2 q_2 \cos x_2 \\ -\dot{x}_1 b \sin x_1 & \dot{q}_2 \cos x_2 + \dot{x}_2 q_2 \sin x_2 \end{bmatrix}$$

$$\mathbf{B} = -\frac{\partial \mathbf{f}}{\partial \mathbf{q}} = -\begin{bmatrix} -a \sin q_1 & -\cos x_2 \\ a \cos q_1 & -\sin x_2 \end{bmatrix}$$

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$$\dot{\mathbf{B}} = \frac{d}{dt} \mathbf{B} = \begin{bmatrix} \dot{q}_1 a \cos q_1 & -\dot{x}_2 \sin x_2 \\ \dot{q}_1 a \sin q_1 & \dot{x}_2 \cos x_2 \end{bmatrix}$$

$$\ddot{\mathbf{x}} = \mathbf{A}^{-1}(-\dot{\mathbf{A}}\dot{\mathbf{x}} + \dot{\mathbf{B}}\dot{\mathbf{q}} + \mathbf{B}\ddot{\mathbf{q}})$$

$$\ddot{\mathbf{x}} = [\ddot{x}_1, \ddot{x}_2]^T \quad \ddot{\mathbf{q}} = [\ddot{q}_1, \ddot{q}_2]^T$$

Acceleration equation

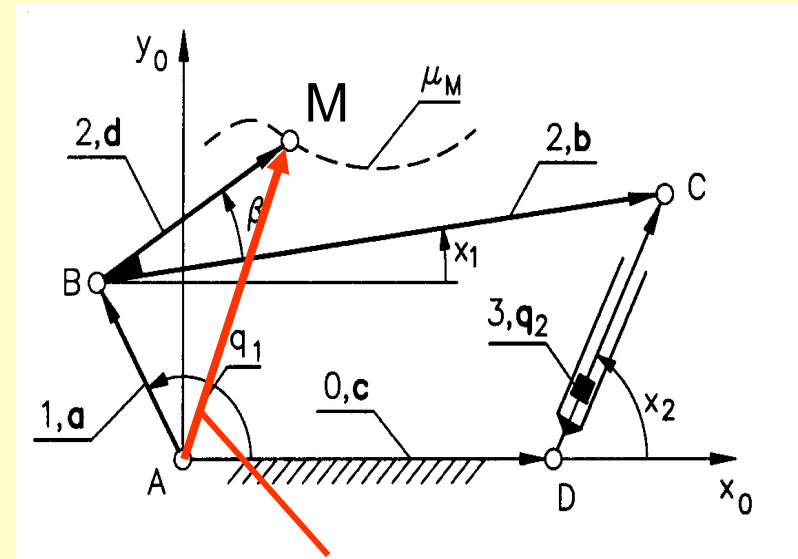
$$\mathbf{B} = -\frac{\partial \mathbf{f}}{\partial \mathbf{q}} = -\begin{bmatrix} -a \sin q_1 & -\cos x_2 \\ a \cos q_1 & -\sin x_2 \end{bmatrix}$$

$$\begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} =$$

$$= \begin{bmatrix} -b \sin x_1 & q_2 \sin x_2 \\ b \cos x_1 & -q_2 \cos x_2 \end{bmatrix}^{-1} \left\{ -\begin{bmatrix} -\dot{x}_1 b \cos x_1 & \dot{q}_2 \sin x_2 - \dot{x}_2 q_2 \cos x_2 \\ -\dot{x}_1 b \sin x_1 & \dot{q}_2 \cos x_2 + \dot{x}_2 q_2 \sin x_2 \end{bmatrix} \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} \right. \\ \left. + \begin{bmatrix} \dot{q}_1 a \cos q_1 & -\dot{x}_2 \sin x_2 \\ \dot{q}_1 a \sin q_1 & \dot{x}_2 \cos x_2 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} + \begin{bmatrix} a \sin q_1 & -\cos x_2 \\ a \cos q_1 & -\sin x_2 \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} \right\}$$

$$\mathbf{r}_M = \mathbf{a} + \mathbf{d}$$

$$\begin{bmatrix} x_M \\ y_M \end{bmatrix} = \begin{bmatrix} a \cos q_1 + d \cos(x_1 + \beta) \\ a \sin q_1 + d \sin(x_1 + \beta) \end{bmatrix}$$



$\mathbf{r}_M$

$$\begin{bmatrix} \dot{x}_M \\ \dot{y}_M \end{bmatrix} = \begin{bmatrix} -a\dot{q}_1 \sin q_1 - d\dot{x}_1 \sin(x_1 + \beta) \\ a\dot{q}_1 \cos q_1 + d\dot{x}_1 \cos(x_1 + \beta) \end{bmatrix}$$

$$\begin{bmatrix} \ddot{x}_M \\ \ddot{y}_M \end{bmatrix} = \begin{bmatrix} -a\ddot{q}_1 \sin q_1 - a\dot{q}_1^2 \cos q_1 - d\ddot{x}_1 \sin(x_1 + \beta) - d\dot{x}_1^2 \cos(x_1 + \beta) \\ a\ddot{q}_1 \cos q_1 - a\dot{q}_1^2 \sin q_1 + d\ddot{x}_1 \cos(x_1 + \beta) - d\dot{x}_1^2 \sin(x_1 + \beta) \end{bmatrix}$$

# MANIPULATORS

(robot mechanisms)

SERIAL and PARALLEL

PLANAR MANIPULATORS



# APPLICATIONS of ROBOTS:

Operation in a danger zone:

- RADIATION
- EXPLOSION (POLICE, ARMY)
- HIGH PRESSURE, HIGH TEMPERATURE

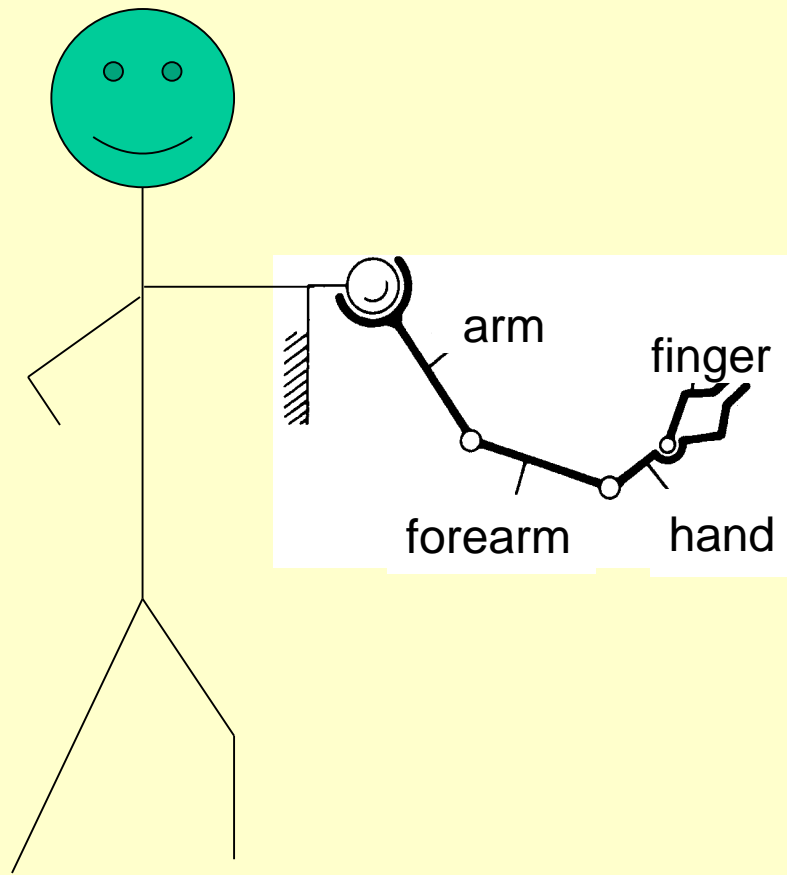
Manufacturing

- ASSAMBLY, WELDING, MACHINING, etc

Health care

- REHABILITATION
- OPERATIONS

and many others ...



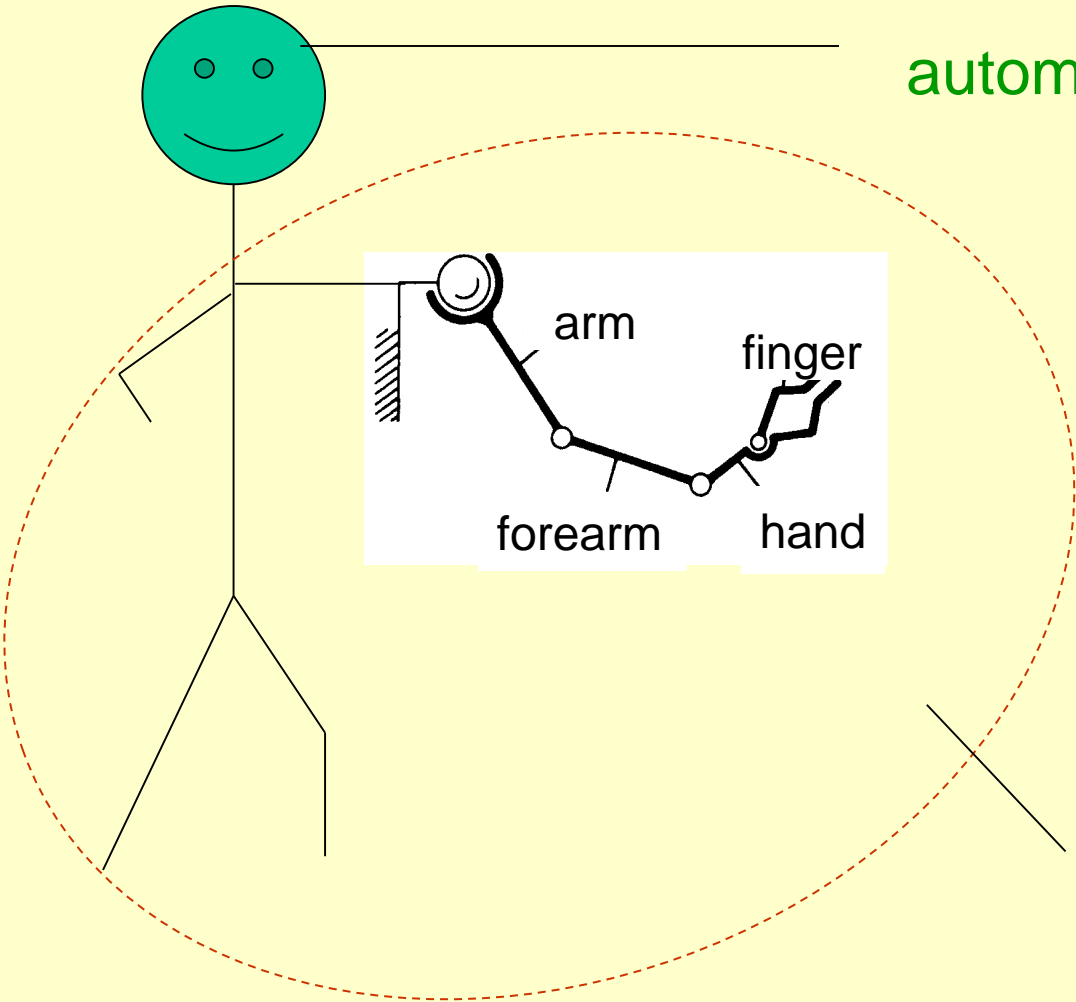
## **END-EFFECTOR**

Device attached to the robot arm by which objects can be grasped or acted upon.

## **MANIPULATOR**

Mechanical device for gripping and the controlled movement of objects (mechanism having many degrees of freedom)

automatic control

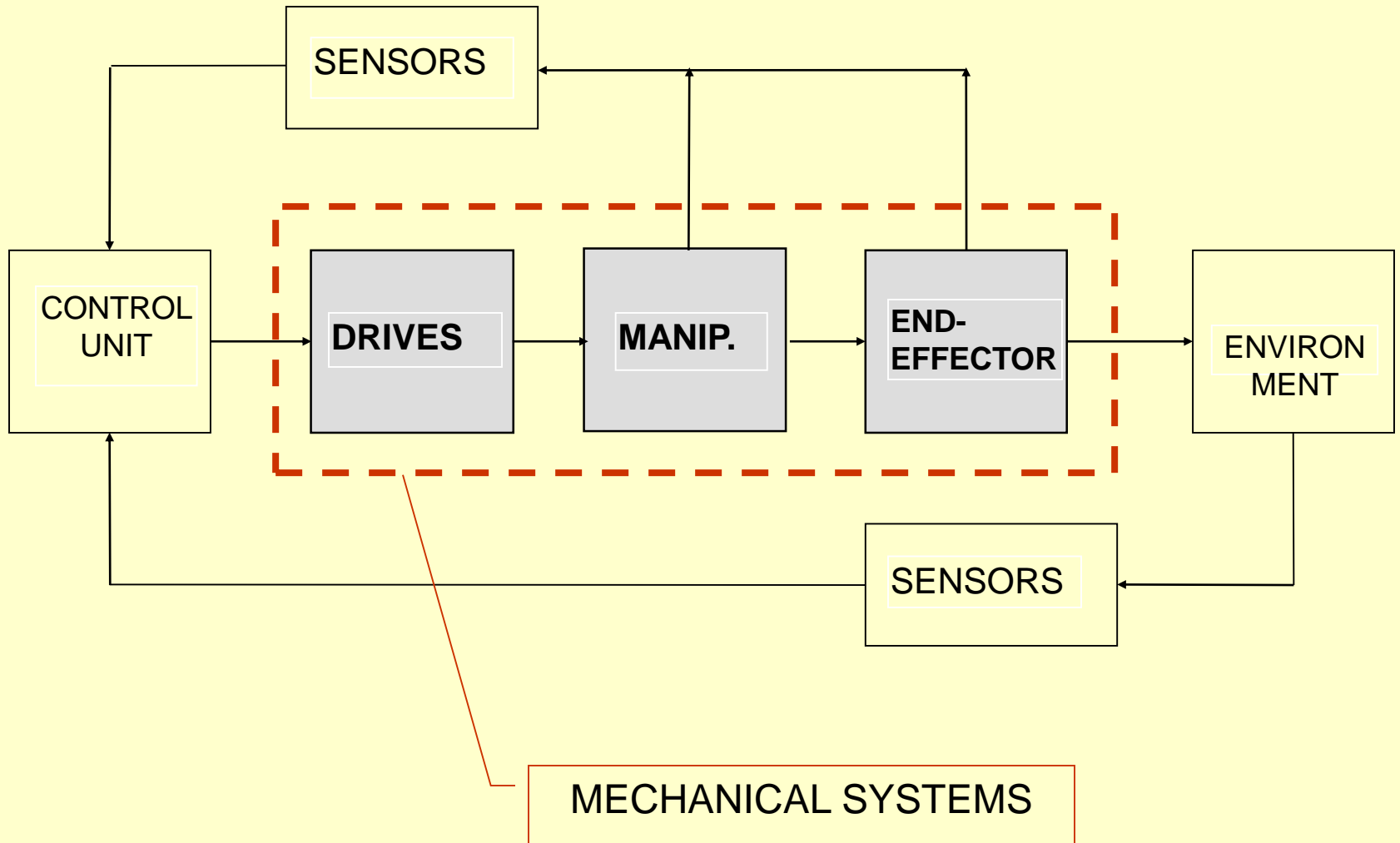


mechanical system

**ROBOT**

Mechanical system under automatic control that performs operations such as handling and locomotion

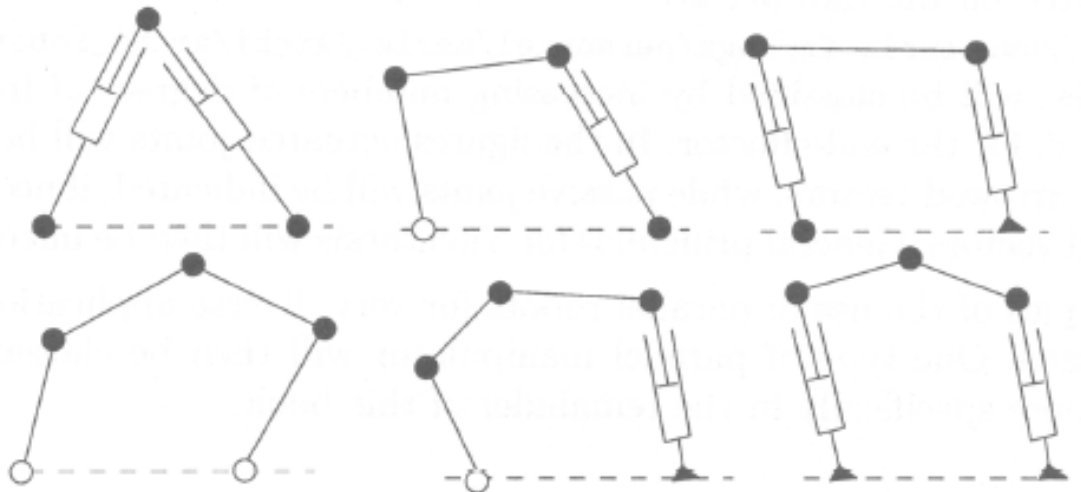
# Modern robot block diagram



# PARALLEL MANIPULATORS

Manipulator that controls the motion of its end effector by means of at least two kinematic chains going from the end-effector towards the frame.

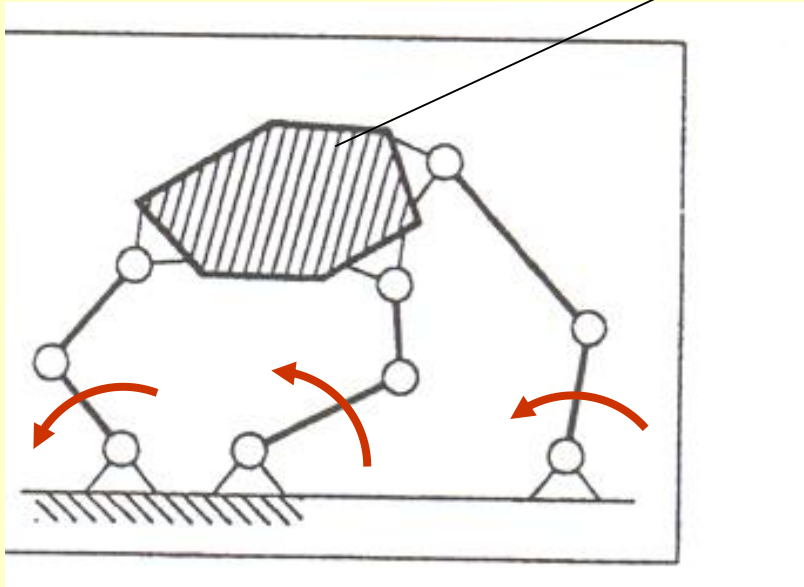
## Planar parallel robot – 2 dof



*Figure 2.1.* Two degrees of freedom planar robots, according to McCloy. White circles represent active revolute joints, black circles passive ones.

# Parallel manipulators (2D)

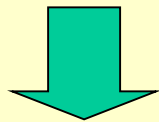
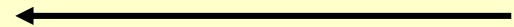
end-effector (platform)



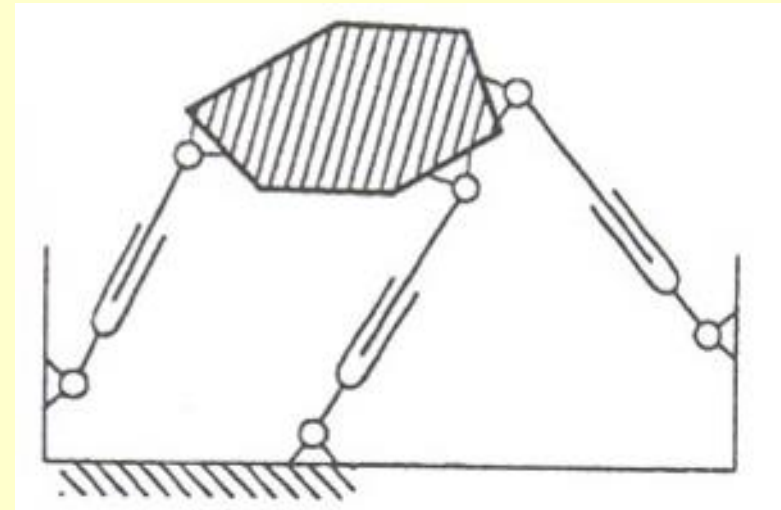
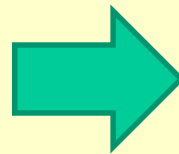
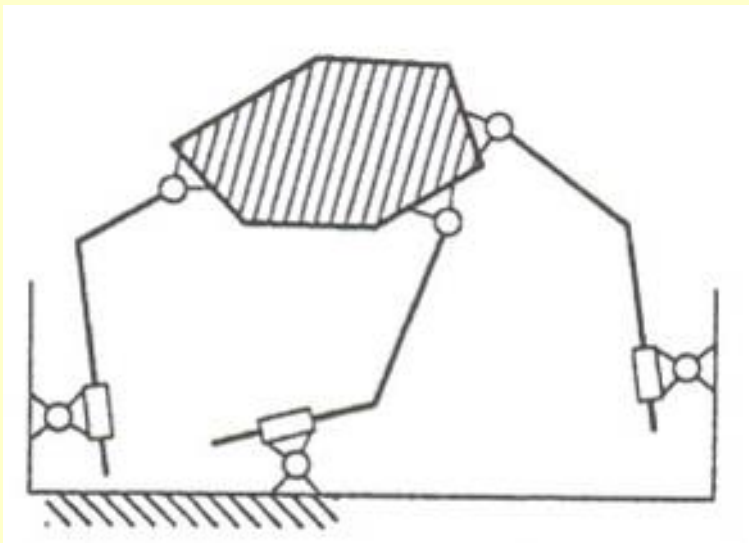
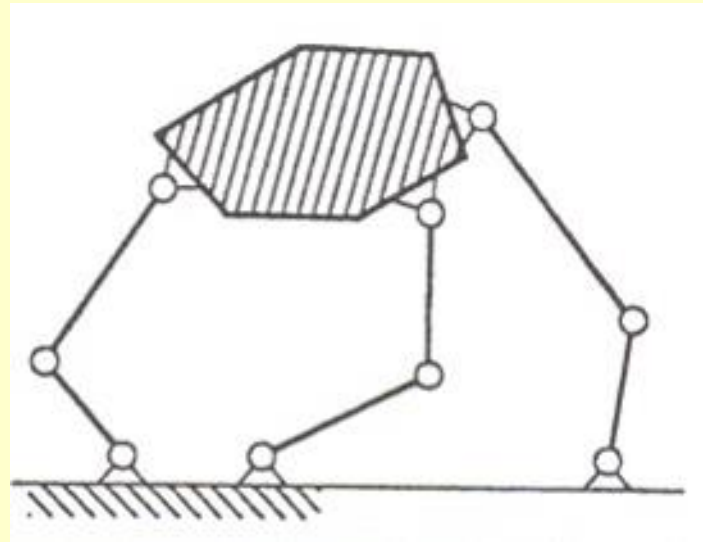
$$\text{DOF} = 3$$

circles are 1-st  
class joints:

R and/or T

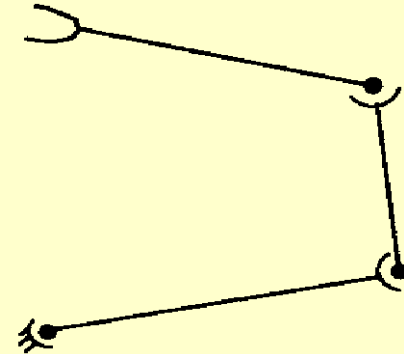


# 3 RRR

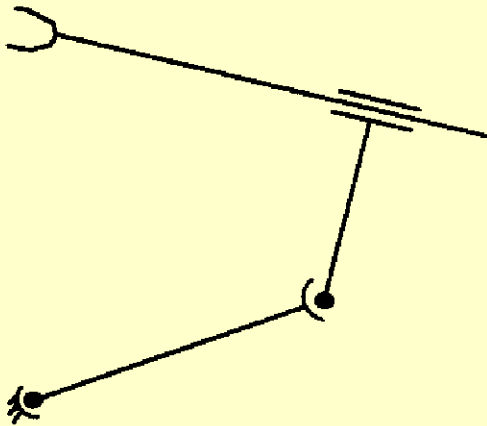


# Planar serial manipulators DOF = 3

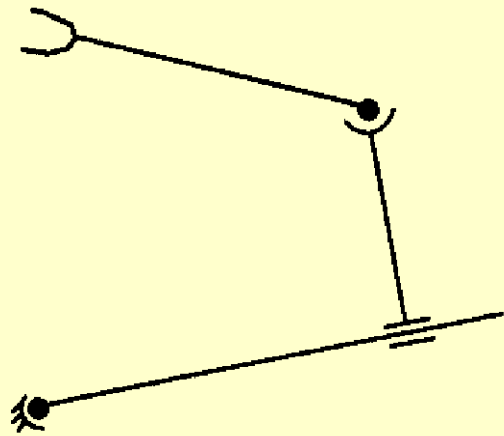
RRR



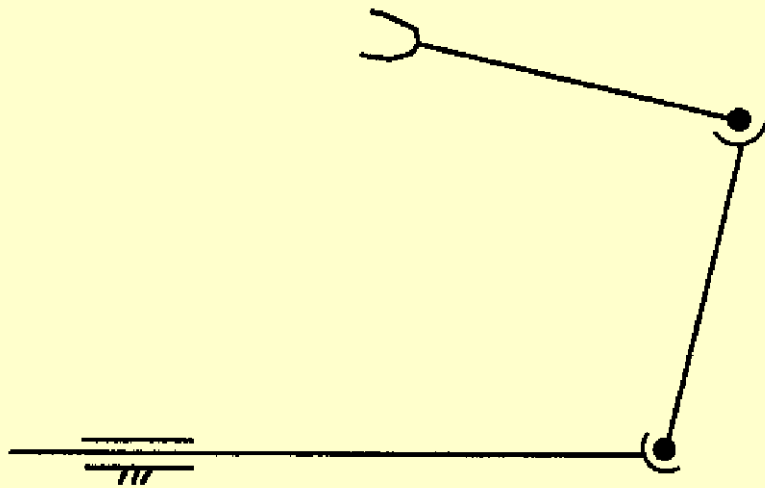
RRT



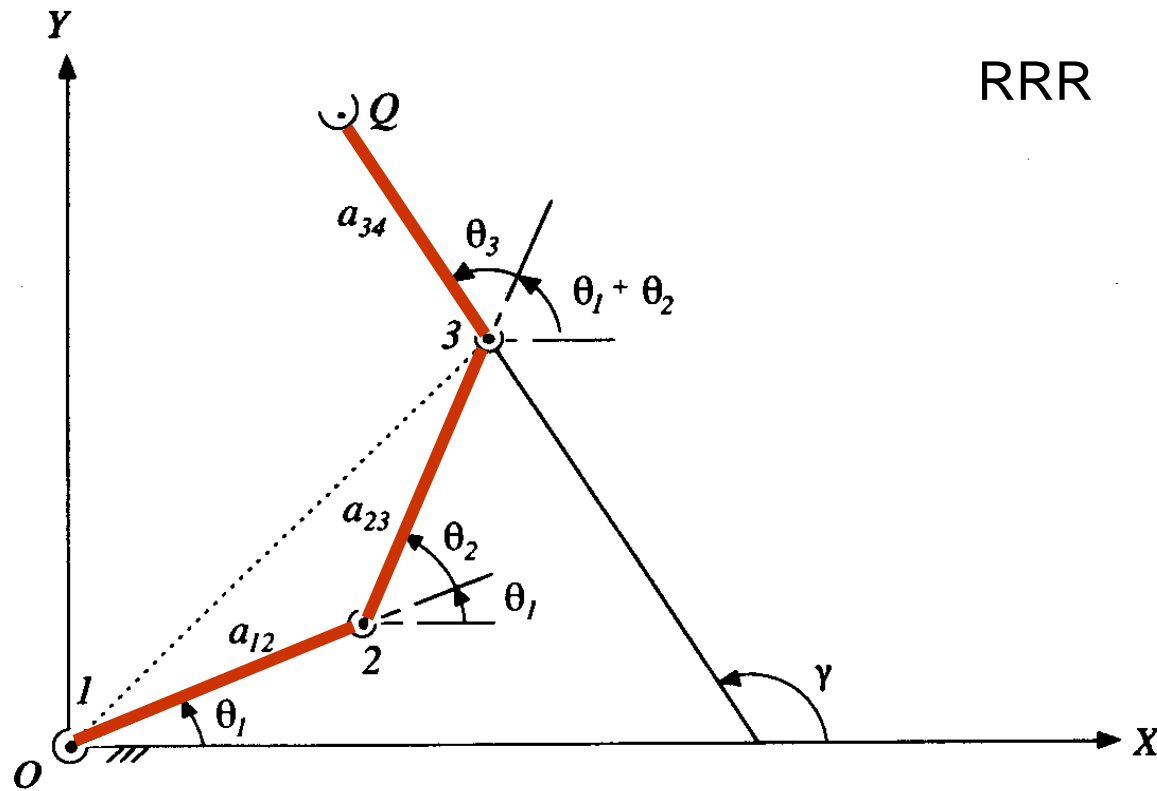




RTR



TRR

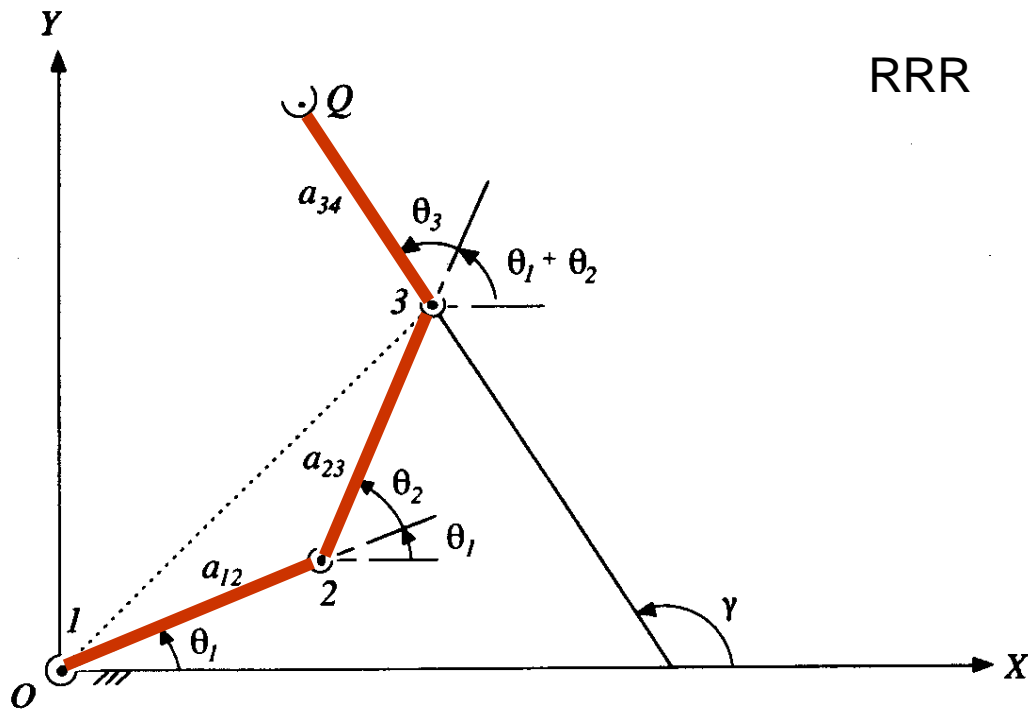


RRR

Direct kinematics: known  $:\theta_1, \theta_2, \theta_3 \rightarrow \begin{cases} x_Q, y_Q - \text{position} \\ \gamma - \text{orientation} \end{cases}$

### In general: DIRECT TASK

Computation of the pose, motion and forces at the end-effector of a robot arm from given actuator displacements, velocities, accelerations and forces

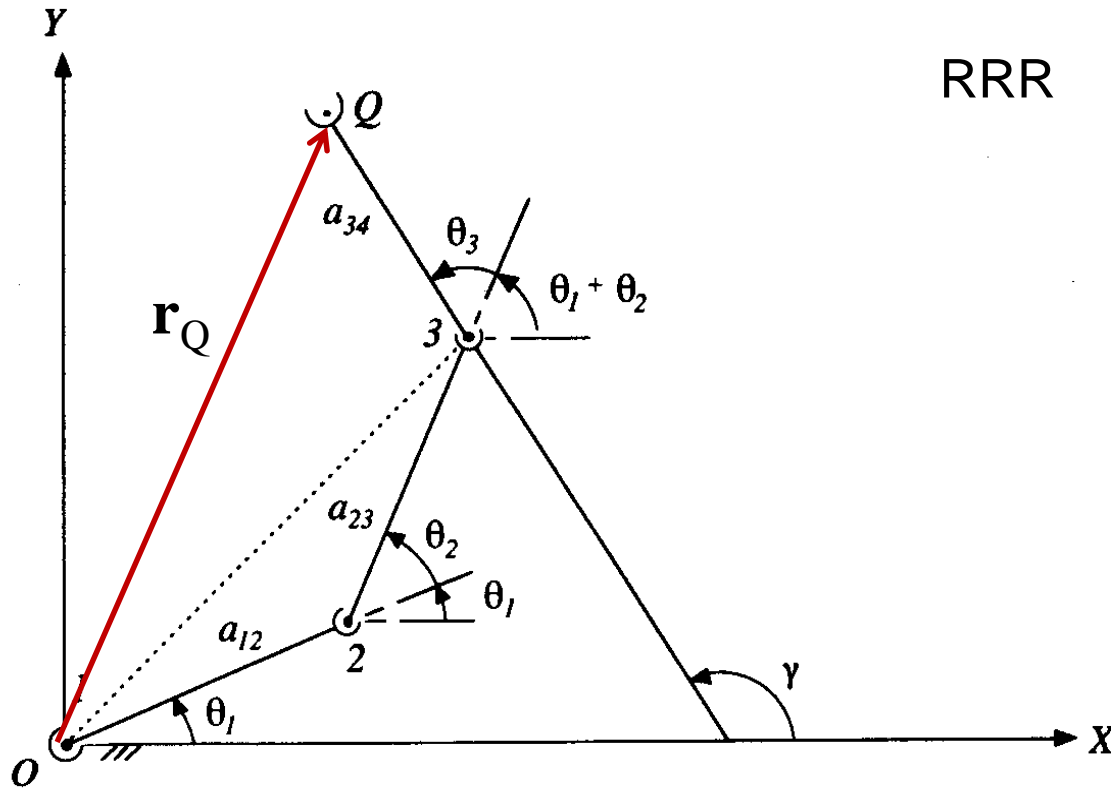


Inverse kinematics: *known* :  $\left\{ \begin{array}{l} x_Q, y_Q - \text{position} \\ \gamma - \text{orientation} \end{array} \right\} \rightarrow \theta_1, \theta_2, \theta_3$

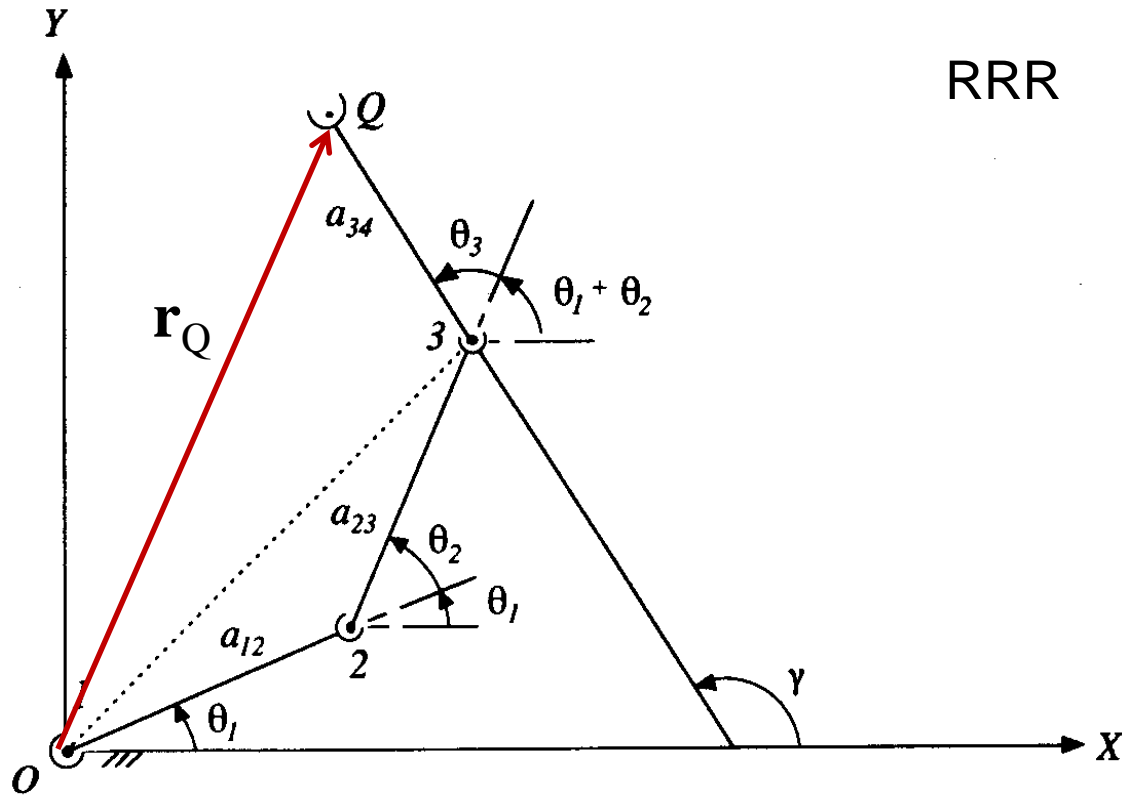
### In general: INVERSE TASK

Computation of actuator forces, displacements, velocities and accelerations from given forces, pose and motion of the end-effector of a robot.

# Direct kinematics using vector projections



$$\mathbf{r}_Q = \mathbf{a}_{12} + \mathbf{a}_{23} + \mathbf{a}_{34} \quad \leftarrow \text{vectors}$$

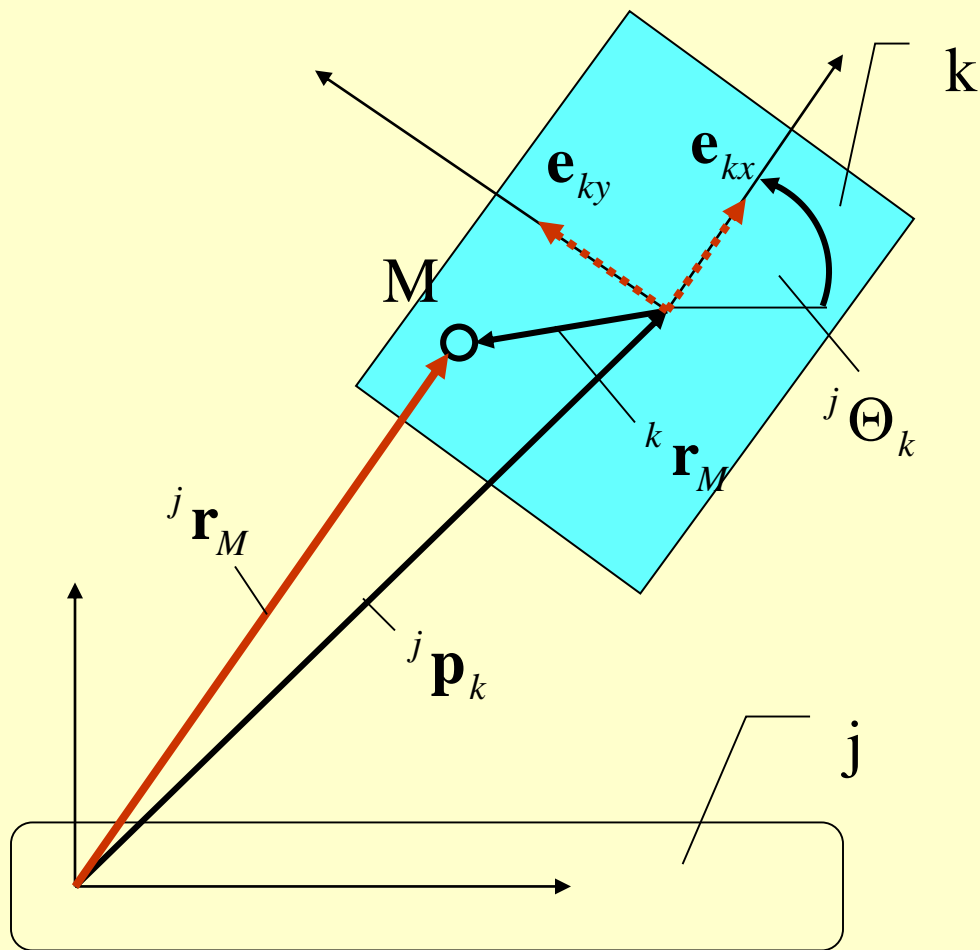


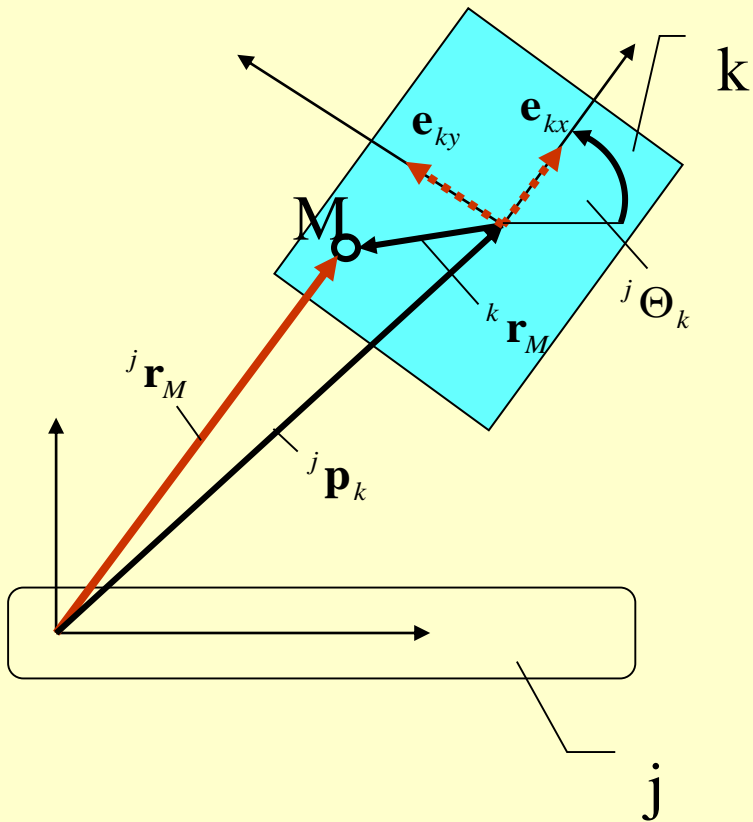
$$x_Q = a_{12} \cos \theta_1 + a_{23} \cos(\theta_1 + \theta_2) + a_{34} \cos(\theta_1 + \theta_2 + \theta_3)$$

$$y_Q = a_{12} \sin \theta_1 + a_{23} \sin(\theta_1 + \theta_2) + a_{34} \sin(\theta_1 + \theta_2 + \theta_3)$$

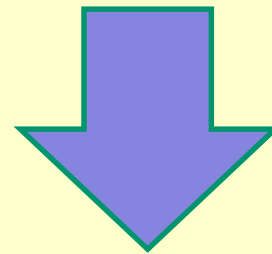
$$\gamma = \theta_1 + \theta_2 + \theta_3$$

*Direct kinematics using Cartesian coordinates (absolute coordinates)*





$${}^j \mathbf{r}_M = {}^j \mathbf{R}_k {}^k \mathbf{r}_M + {}^j \mathbf{p}_k$$



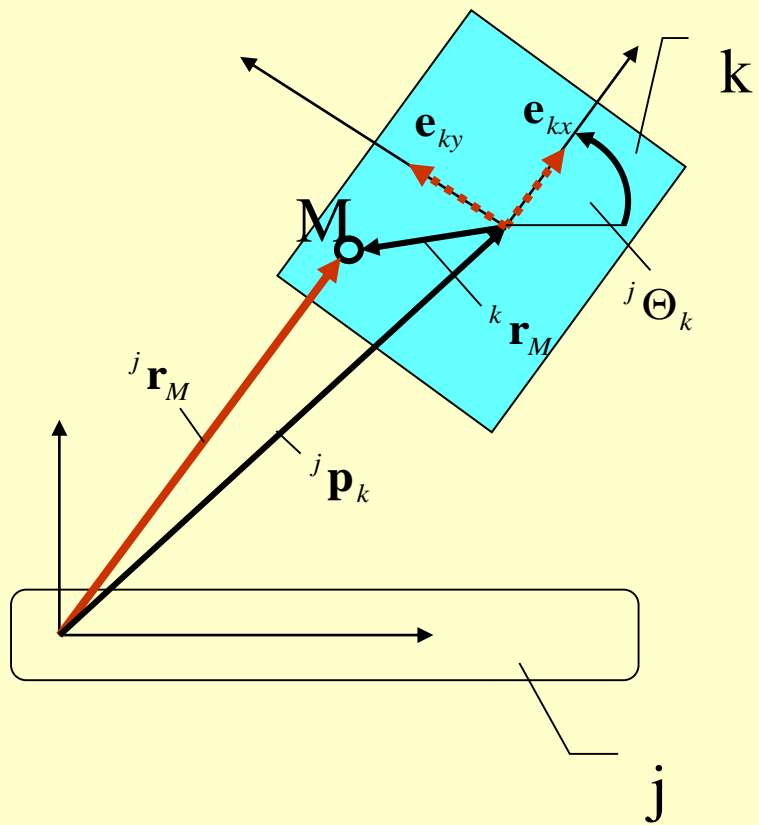
Rotation matrix

$${}^j \mathbf{R}_k = \begin{bmatrix} {}^j \mathbf{e}_{kx} & {}^j \mathbf{e}_{ky} \end{bmatrix} = \begin{bmatrix} \cos {}^j \Theta_k & -\sin {}^j \Theta_k \\ \sin {}^j \Theta_k & \cos {}^j \Theta_k \end{bmatrix}$$

versors

$${}^j \mathbf{e}_{kx} = \begin{bmatrix} \cos {}^j \Theta_k \\ \sin {}^j \Theta_k \end{bmatrix}$$

$${}^j \mathbf{e}_{ky} = \begin{bmatrix} -\sin {}^j \Theta_k \\ \cos {}^j \Theta_k \end{bmatrix}$$



$$\begin{bmatrix} {}^j x_M \\ {}^j y_M \end{bmatrix} = \begin{bmatrix} \cos {}^j \Theta_k & -\sin {}^j \Theta_k \\ \sin {}^j \Theta_k & \cos {}^j \Theta_k \end{bmatrix} \begin{bmatrix} {}^k x_M \\ {}^k y_M \end{bmatrix} + \begin{bmatrix} {}^j x_k \\ {}^j y_k \end{bmatrix}$$



# Properties of rotation matrix

Inversion=transposition!!!

$${}^j\mathbf{R}_k^{-1} = {}^j\mathbf{R}_k^T = \begin{bmatrix} \cos {}^j\Theta_k & \sin {}^j\Theta_k \\ -\sin {}^j\Theta_k & \cos {}^j\Theta_k \end{bmatrix}$$

$${}^j\mathbf{R}_k {}^j\mathbf{R}_k^{-1} = \begin{bmatrix} \cos {}^j\Theta_k & -\sin {}^j\Theta_k \\ \sin {}^j\Theta_k & \cos {}^j\Theta_k \end{bmatrix} \begin{bmatrix} \cos {}^j\Theta_k & \sin {}^j\Theta_k \\ -\sin {}^j\Theta_k & \cos {}^j\Theta_k \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} = \mathbf{I}$$



identity matrix

Instead of

$${}^j \mathbf{r}_M = {}^j \mathbf{R}_k {}^k \mathbf{r}_M + {}^j \mathbf{p}_k$$

we can use

$${}^j \mathbf{r}_M = {}^j \mathbf{A}_k {}^k \mathbf{r}_M$$

Homogeneous transformation

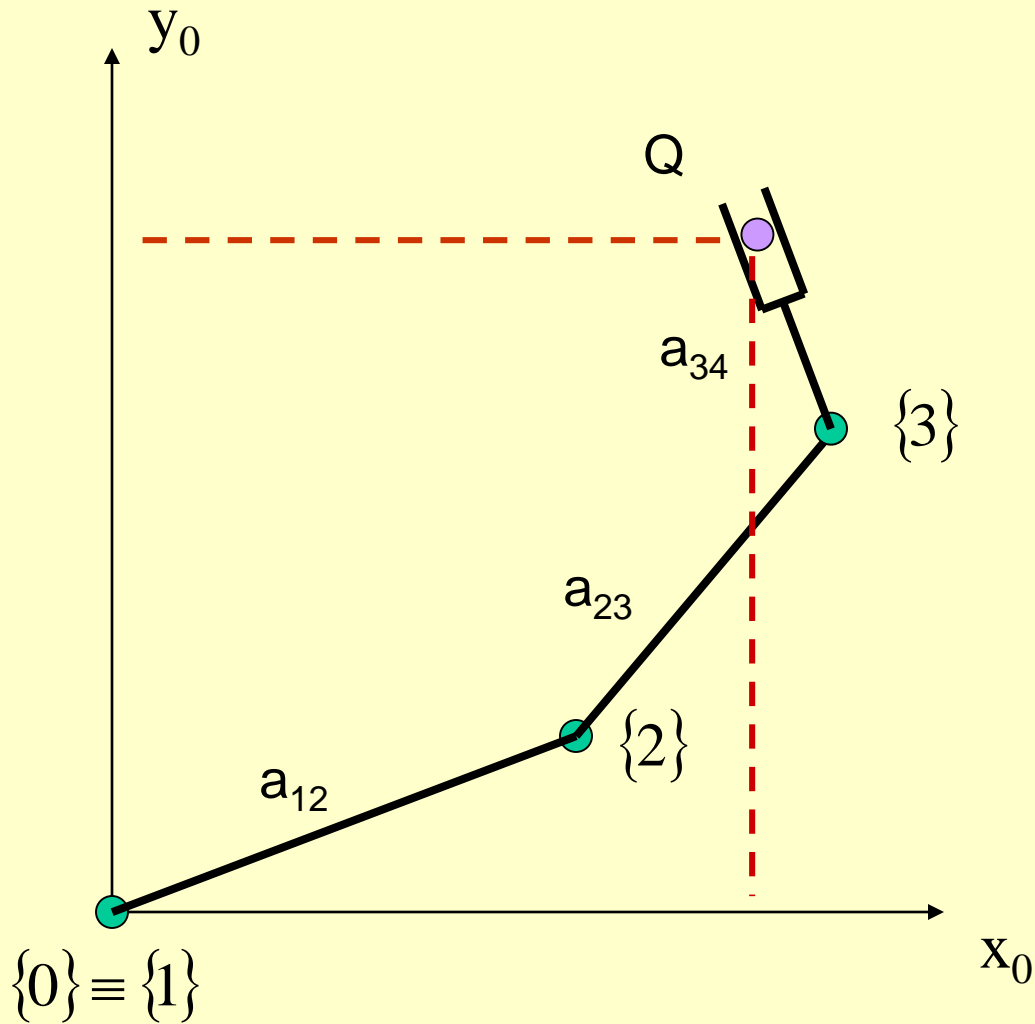
$${}^j \mathbf{A}_k = \begin{bmatrix} {}^j \mathbf{R}_k & {}^j \mathbf{p}_k \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^j \mathbf{A}_k = \begin{bmatrix} \cos {}^j \Theta_k & -\sin {}^j \Theta_k & {}^j x_k \\ \sin {}^j \Theta_k & \cos {}^j \Theta_k & {}^j y_k \\ 0 & 0 & 1 \end{bmatrix}$$

Vector of cart. coordinates

$${}^j \mathbf{q}_k = \left[ {}^j \mathbf{p}_k^T \quad {}^j \Theta_k \right]^T = \left[ {}^j x_k \quad {}^j y_k \quad {}^j \Theta_k \right]^T$$

## Example



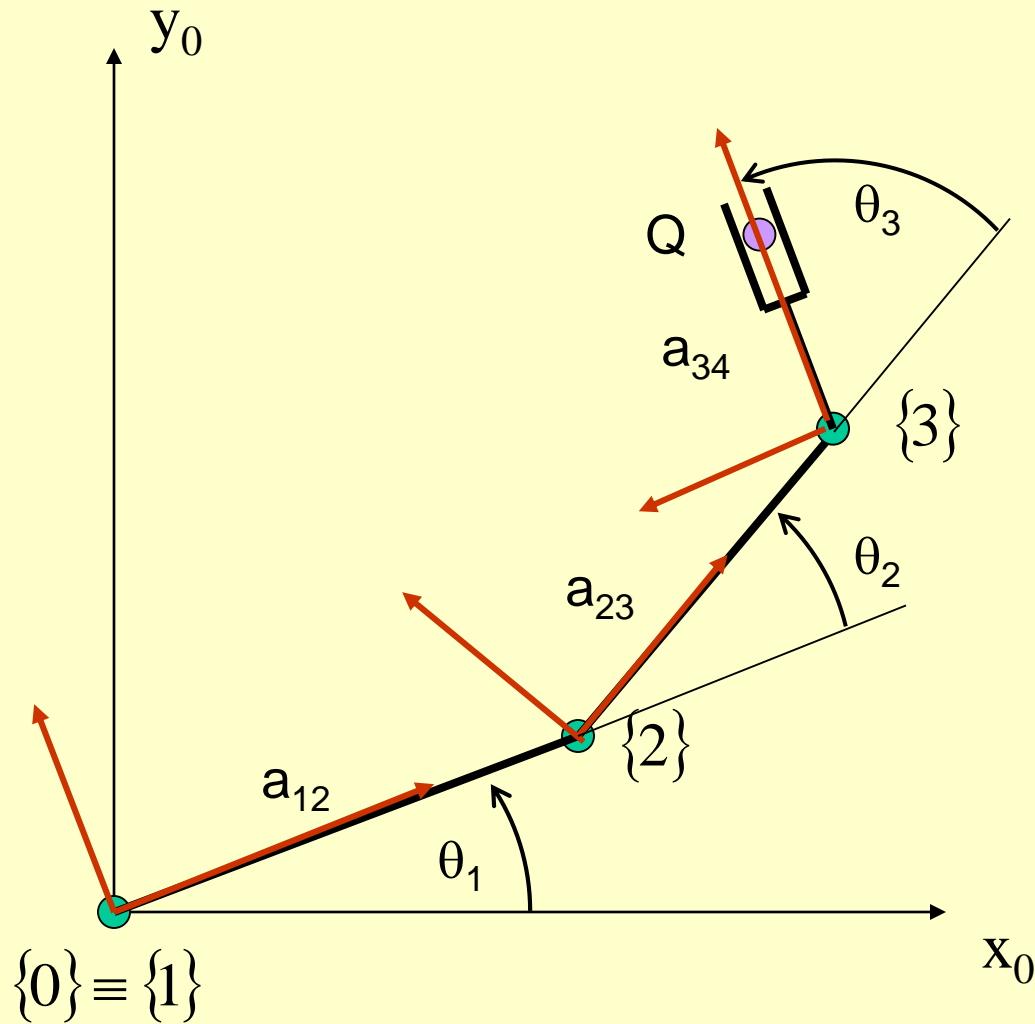
### Known:

point  $Q$  position on link 3  
link dimensions  
joint variables

### Find:

point  $Q$  position in frame  
coordinate system  $x_0y_0$

## Example



1. Introduce link coordinate systems and joint variables

2. equations

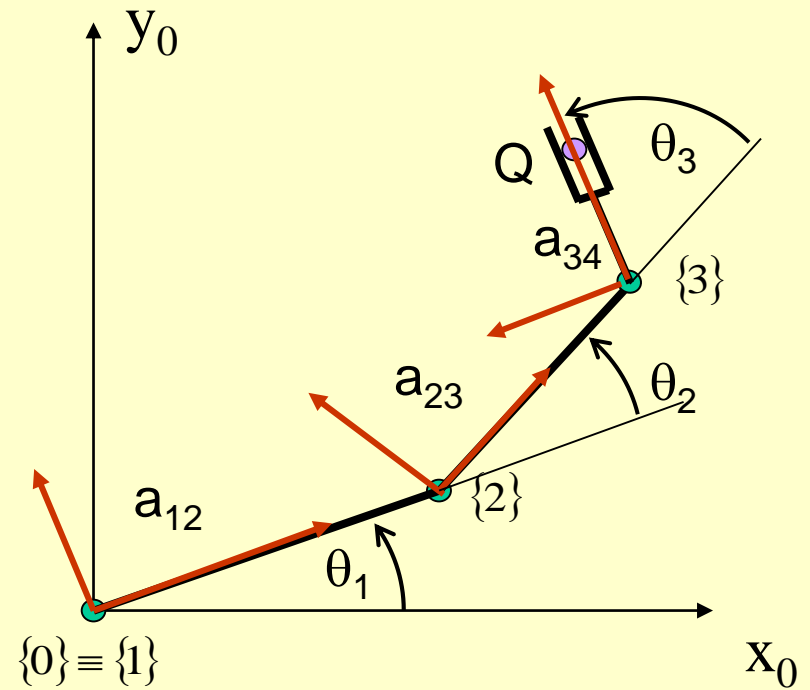
$$\begin{bmatrix} {}^3x_Q \\ {}^3y_Q \\ 1 \end{bmatrix} = \begin{bmatrix} a_{34} \\ 0 \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} x_Q \\ y_Q \\ 1 \end{bmatrix} = {}^0A_1 \cdot {}^1A_2 \cdot {}^2A_3 \begin{bmatrix} {}^3x_Q \\ {}^3y_Q \\ 1 \end{bmatrix}$$

$${}^0\mathbf{A}_1 = \begin{bmatrix} \cos \Theta_1 & -\sin \Theta_1 & 0 \\ \sin \Theta_1 & \cos \Theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^1\mathbf{A}_2 = \begin{bmatrix} \cos \Theta_2 & -\sin \Theta_2 & a_{12} \\ \sin \Theta_2 & \cos \Theta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

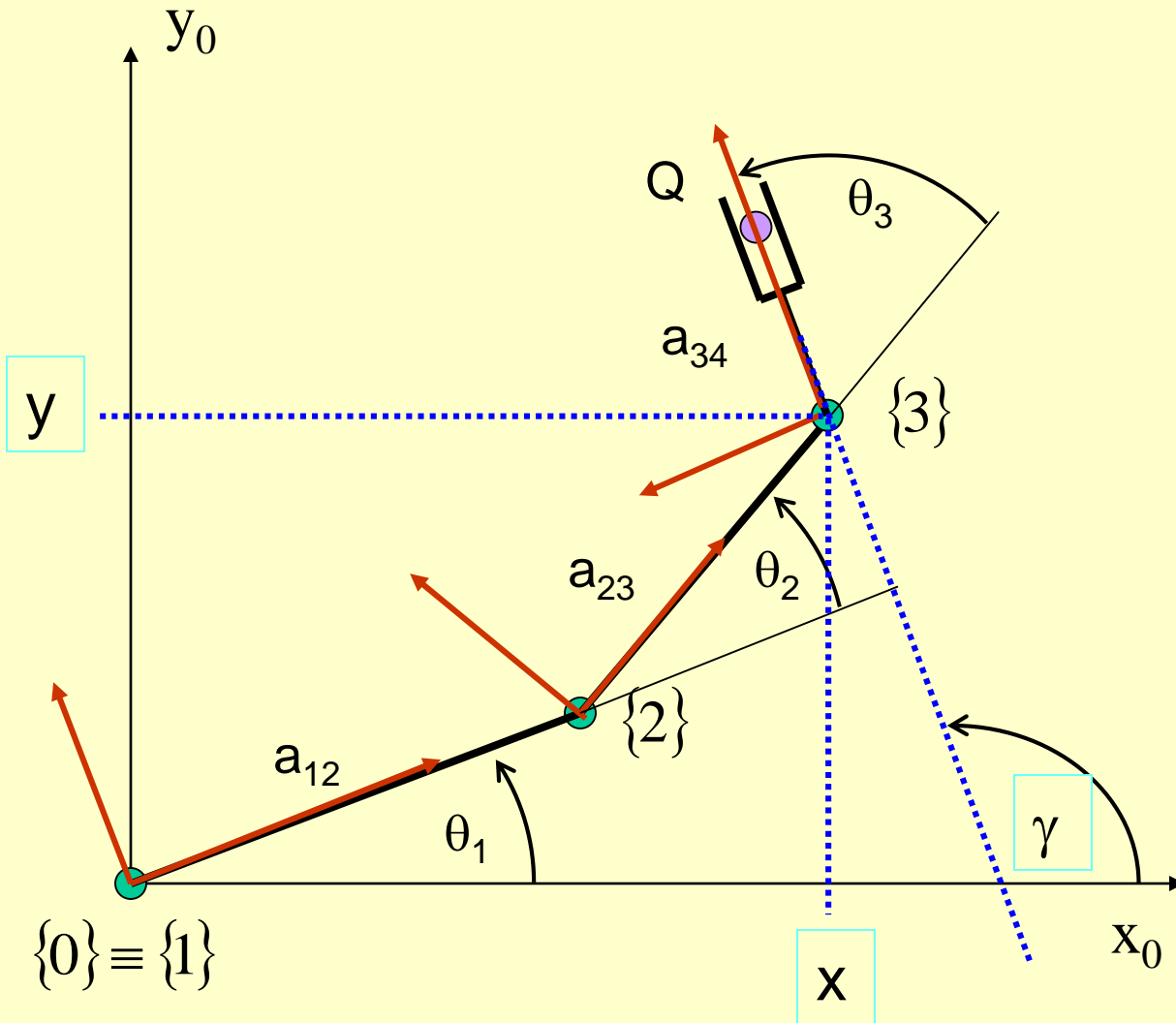
$${}^2\mathbf{A}_3 = \begin{bmatrix} \cos \Theta_3 & -\sin \Theta_3 & a_{23} \\ \sin \Theta_3 & \cos \Theta_3 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



$$\begin{bmatrix} x_Q \\ y_Q \\ 1 \end{bmatrix} = \begin{bmatrix} \cos \Theta_1 & -\sin \Theta_1 & 0 \\ \sin \Theta_1 & \cos \Theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} \cos \Theta_2 & -\sin \Theta_2 & a_{12} \\ \sin \Theta_2 & \cos \Theta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \cdot \begin{bmatrix} \cos \Theta_3 & -\sin \Theta_3 & a_{23} \\ \sin \Theta_3 & \cos \Theta_3 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} {}^3x_Q \\ {}^3y_Q \\ 1 \end{bmatrix}$$

Manipulator 2D

Inverse kinematics

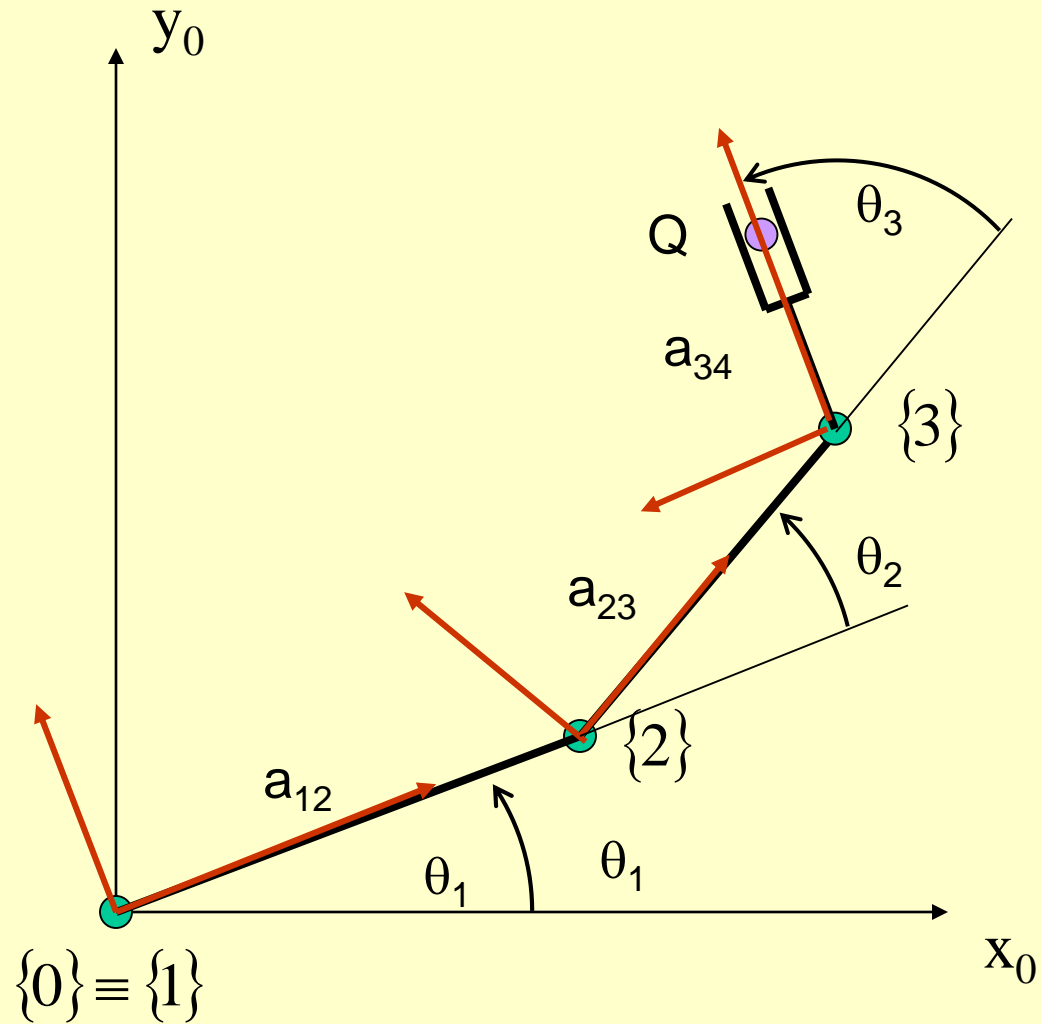


Given:

$x, y, \gamma$

Calculate:

$\Theta_i = ?, i = 1, 2, 3$



We already have:

$$\begin{bmatrix} x_Q \\ y_Q \\ 1 \end{bmatrix} = {}^0\mathbf{A}_1 \cdot {}^1\mathbf{A}_2 \cdot {}^2\mathbf{A}_3 \begin{bmatrix} {}^3x_Q \\ {}^3y_Q \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} {}^3x_Q \\ {}^3y_Q \\ 1 \end{bmatrix} = \begin{bmatrix} a_{34} \\ 0 \\ 1 \end{bmatrix}$$



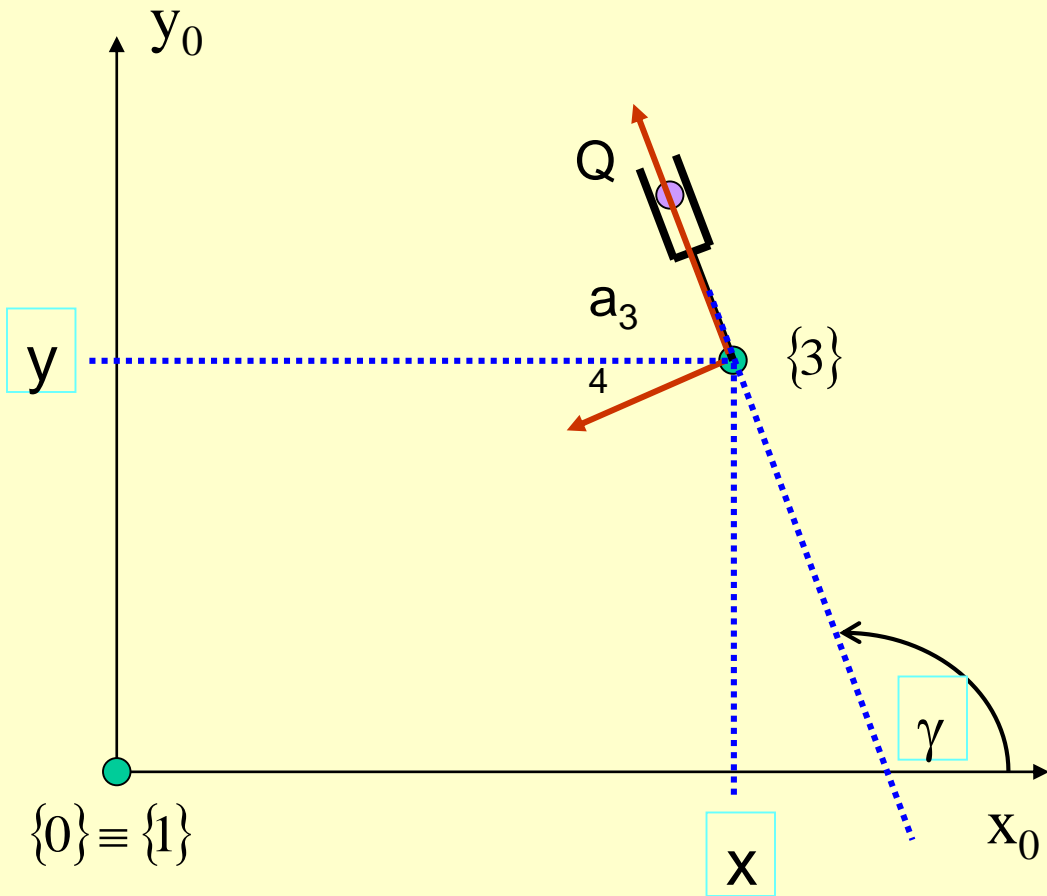
$${}^0\mathbf{A}_1 = \begin{bmatrix} \cos \Theta_1 & -\sin \Theta_1 & 0 \\ \sin \Theta_1 & \cos \Theta_1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^1\mathbf{A}_2 = \begin{bmatrix} \cos \Theta_2 & -\sin \Theta_2 & a_{12} \\ \sin \Theta_2 & \cos \Theta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^2\mathbf{A}_3 = \begin{bmatrix} \cos \Theta_3 & -\sin \Theta_3 & a_{23} \\ \sin \Theta_3 & \cos \Theta_3 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^0\mathbf{A}_1 \cdot {}^1\mathbf{A}_2 \cdot {}^2\mathbf{A}_3 = {}^0\mathbf{A}_3$$

$${}^0\mathbf{A}_3 = \begin{bmatrix} \cos(\Theta_1 + \Theta_2 + \Theta_3) & -\sin(\Theta_1 + \Theta_2 + \Theta_3) & a_{12} \cos \Theta_1 + a_{23} \cos(\Theta_1 + \Theta_2) \\ \sin(\Theta_1 + \Theta_2 + \Theta_3) & \cos(\Theta_1 + \Theta_2 + \Theta_3) & a_{12} \sin \Theta_1 + a_{23} \sin(\Theta_1 + \Theta_2) \\ 0 & 0 & 1 \end{bmatrix}$$



$${}^0\mathbf{T}_3 = \begin{bmatrix} \cos \gamma & -\sin \gamma & x \\ \sin \gamma & \cos \gamma & y \\ 0 & 0 & 1 \end{bmatrix}$$

$${}^0\mathbf{A}_3 = \begin{bmatrix} \cos(\Theta_1 + \Theta_2 + \Theta_3) & -\sin(\Theta_1 + \Theta_2 + \Theta_3) & a_{12} \cos \Theta_1 + a_{23} \cos(\Theta_1 + \Theta_2) \\ \sin(\Theta_1 + \Theta_2 + \Theta_3) & \cos(\Theta_1 + \Theta_2 + \Theta_3) & a_{12} \sin \Theta_1 + a_{23} \sin(\Theta_1 + \Theta_2) \\ 0 & 0 & 1 \end{bmatrix}$$


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Comparison of matrices:

$${}^0\mathbf{A}_3 = {}^0\mathbf{T}_3 = \begin{bmatrix} \cos \gamma & -\sin \gamma & x \\ \sin \gamma & \cos \gamma & y \\ 0 & 0 & 1 \end{bmatrix}$$

It gives 4 equations

$$\left\{ \begin{array}{l} \cos \gamma = \cos(\Theta_1 + \Theta_2 + \Theta_3) \\ \sin \gamma = \sin(\Theta_1 + \Theta_2 + \Theta_3) \\ x = a_{12} \cos \Theta_1 + a_{23} \cos(\Theta_1 + \Theta_2) \\ y = a_{12} \sin \Theta_1 + a_{23} \sin(\Theta_1 + \Theta_2) \end{array} \right. \quad \begin{array}{l} (a) \\ (b) \\ (c) \\ (d) \end{array}$$

$$\Theta_1 = \dots \quad \Theta_2 = \dots \quad \Theta_3 = \dots$$

$$\begin{cases} \cos \gamma = \cos(\Theta_1 + \Theta_2 + \Theta_3) & (a) \\ \sin \gamma = \sin(\Theta_1 + \Theta_2 + \Theta_3) & (b) \\ x = a_{12} \cos \Theta_1 + a_{23} \cos(\Theta_1 + \Theta_2) & (c) \\ y = a_{12} \sin \Theta_1 + a_{23} \sin(\Theta_1 + \Theta_2) & (d) \end{cases}$$


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• (c)<sup>2</sup> and (d)<sup>2</sup> sum gives:

$$x^2 + y^2 = a_{12}^2 + a_{23}^2 + 2a_{12}a_{23}u$$

where:

$$u = \cos \Theta_1 \cos(\Theta_1 + \Theta_2) + \sin \Theta_1 \sin(\Theta_1 + \Theta_2)$$

$$u = \cos \Theta_1 \cos(\Theta_1 + \Theta_2) + \sin \Theta_1 \sin(\Theta_1 + \Theta_2)$$

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Using:

$$\cos(\Theta_1 + \Theta_2) = \cos \Theta_1 \cos \Theta_2 - \sin \Theta_1 \sin \Theta_2$$

$$\sin(\Theta_1 + \Theta_2) = \sin \Theta_1 \cos \Theta_2 + \cos \Theta_1 \sin \Theta_2$$

$$u = \cos \Theta_1 \cos(\Theta_1 + \Theta_2) + \sin \Theta_1 \sin(\Theta_1 + \Theta_2)$$

---

One can obtain

$$\begin{aligned} u &= \cos \Theta_1 \cos \Theta_1 \cos \Theta_2 - \cos \Theta_1 \sin \Theta_1 \sin \Theta_2 + \\ &\quad + \sin \Theta_1 \sin \Theta_1 \cos \Theta_2 + \sin \Theta_1 \cos \Theta_1 \sin \Theta_2 = \\ &= (\cos^2 \Theta_1 + \sin^2 \Theta_1) \cos \Theta_2 = \cos \Theta_2 \end{aligned}$$

$$u = \cos \Theta_2$$



$$x^2 + y^2 = a_{12}^2 + a_{23}^2 + 2a_{12}a_{23}u$$

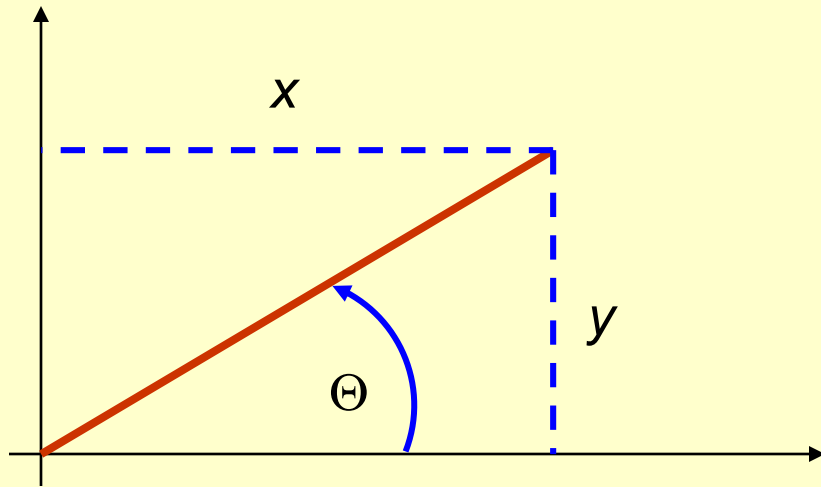
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$$x^2 + y^2 = a_{12}^2 + a_{23}^2 + 2a_{12}a_{23} \cos \Theta_2$$

$$\cos \Theta_2 = \frac{x^2 + y^2 - a_{12}^2 - a_{23}^2}{2a_{12}a_{23}}$$

$$\Theta_2 = \text{atan2}\left(\pm \sqrt{1 - \cos^2 \Theta_2}, \cos \Theta_2\right)$$

# Function $\text{atan2}(y,x) - (1)$



$$-\pi \leq \text{atan2}(y,x) \leq \pi$$

$$\text{atan2}(2,2) = \pi/4$$

$$\text{atan2}(-2,-2) = -3\pi/4$$

but

$$\arctan(2/2) =$$

$$\arctan[(-2)/(-2)] = \pi/4$$

**$\text{atan2}(y,x)$  calculates  $\arctan(y/x)$  for any  $y, x$**

$$\begin{cases} \sin \Theta = a \\ \cos \Theta = b \end{cases} \rightarrow \Theta = \text{atan2}(a, b)$$

$$a \cos \Theta + b \sin \Theta = 0$$

↓

1.  $\Theta = \text{atan2}(a, -b)$
2.  $\Theta = \text{atan2}(-a, b)$

$$\left. \begin{aligned} a \cos \Theta - b \sin \Theta &= c \\ a \sin \Theta + b \cos \Theta &= d \end{aligned} \right\} \rightarrow$$
$$\Theta = \operatorname{atan2}(ad - bc, ac - bd)$$

## Two configurations

$$\Theta_2 = \text{atan2}\left(\pm \sqrt{1 - \cos^2 \Theta_2}, \cos \Theta_2\right)$$

